



# SM quadrupole magnet

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Fermilab

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BERKELEY LAB

Superconducting Magnet Group



# Outline

- Motivations and goals
- SM quadrupole magnet: design features
- Superconducting cable and coil
- Magnetic analysis
- Mechanical analysis
- Conclusions



# Motivations and goals

- Provide early ***feedback*** for IR quadrupole design
  - Support ***structure***
  - Lorentz ***force*** distribution
    - $F_y$  towards the mid-plane
    - $F_x$  outwards
    - High end forces
- Optimize ***assembly procedures***
- Measure the ***mechanical behavior*** of the structure during assembly, cool-down and excitation



# Motivations and goals (cont.)

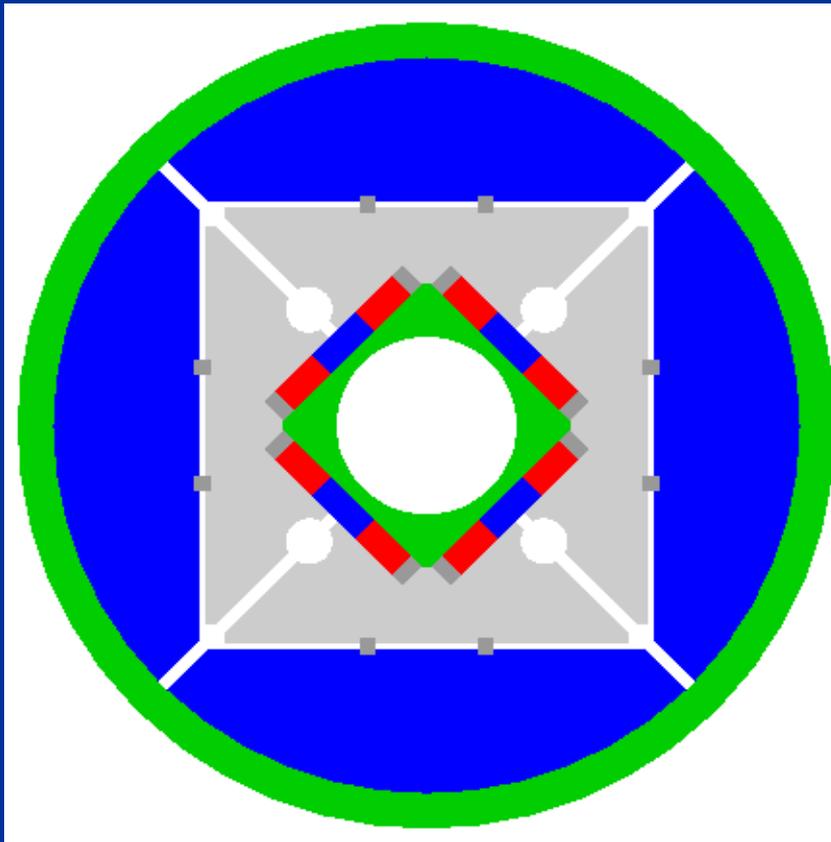
- Cost-effective ***technology development***
  - ***Training studies***
    - Strain gauges attached to the coils
  - Coil ***stress limit*** analysis
  - ***Thermal*** and ***quench protection*** studies
  - Analysis of ***fabrication tolerances*** for Nb<sub>3</sub>Sn coils
    - Accuracy and reproducibility of coil fabrication
    - Accuracy and reproducibility of magnet assembly
    - Simultaneous control of pre-stress and coil size
    - Field corrections: coil shims, magnetic shims
  - ***Alignment*** studies



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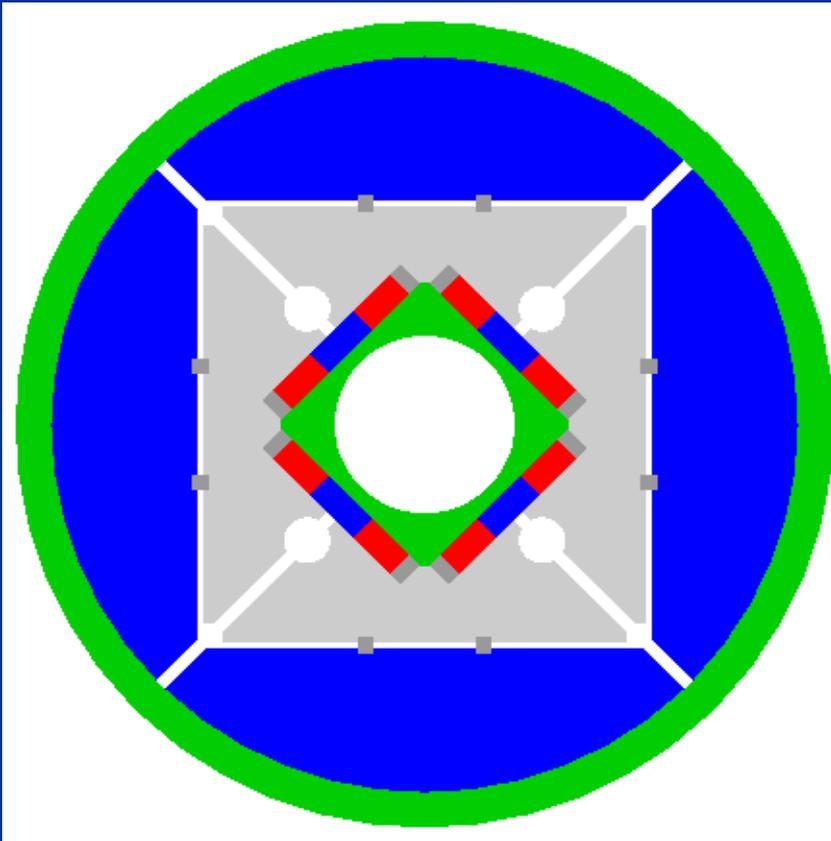
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# Cross-section



- Magnet components
  - Aluminum *shell*
    - Outer diameter: 500 mm
  - 4-piece iron *yoke*
  - Stainless steel *pads*
  - SM racetrack *coils*
  - Aluminum *bore*
- *Keys* and *bladders* technology

# Performance parameters



- Coil aperture  
– 120 mm
- Bore aperture  
– 110 mm
- $I = 11000 \text{ A}$
- $G = 95 \text{ T/m}$
- $B_{\text{peak}} = 11 \text{ T}$
- $U = 425 \text{ KJ/m}$
- $L = 7 \text{ mH/m}$



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# Superconducting cable and coil

- **Conductor**
  - 20 strands ( $\varnothing$  0.7 mm)
  - $8 \times 1.3$  mm
  - 0.1 mm insulation
- **Coil**
  - Two layers
  - 21 turns per layer
  - Straight section: 150 mm
- Iron *island*
- Stainless steel *horseshoe*
- Stainless steel *end shoe*



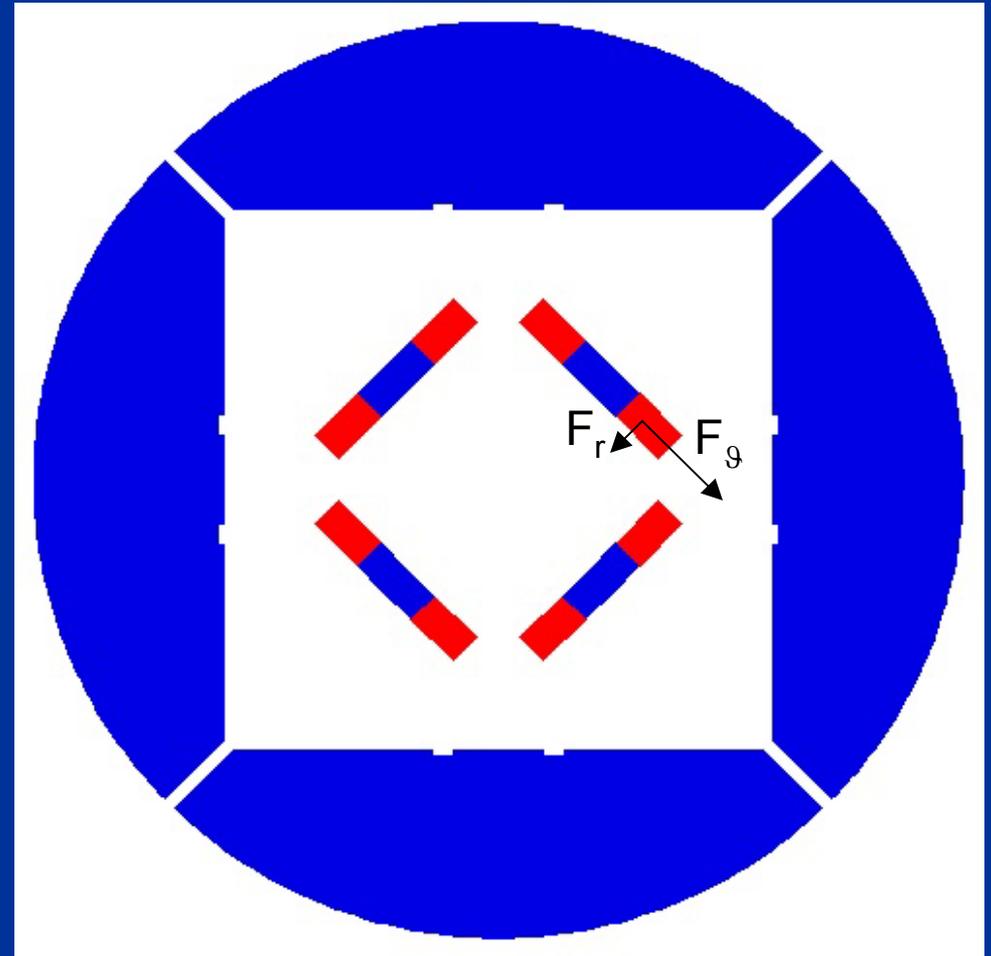


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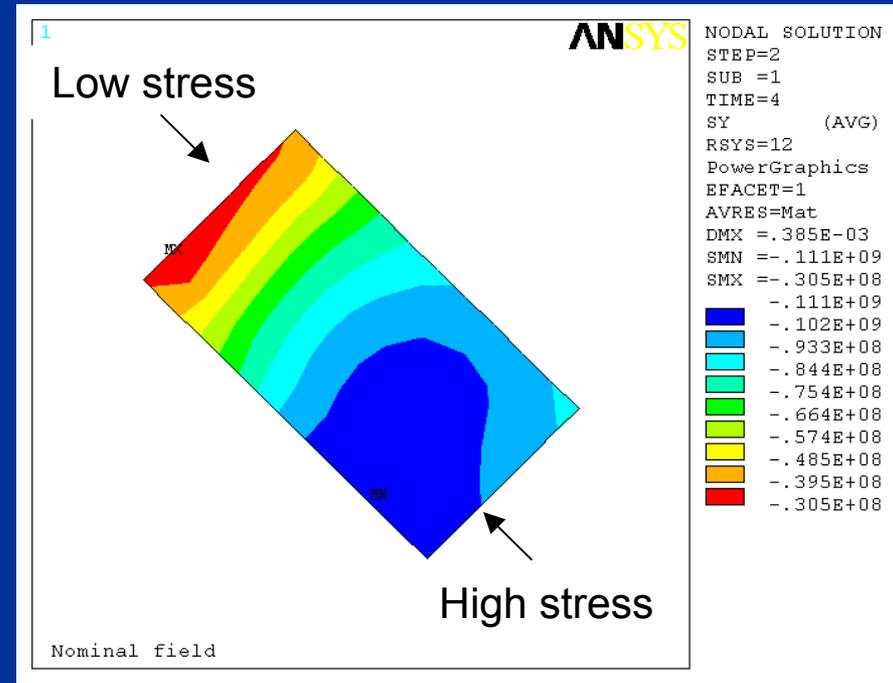
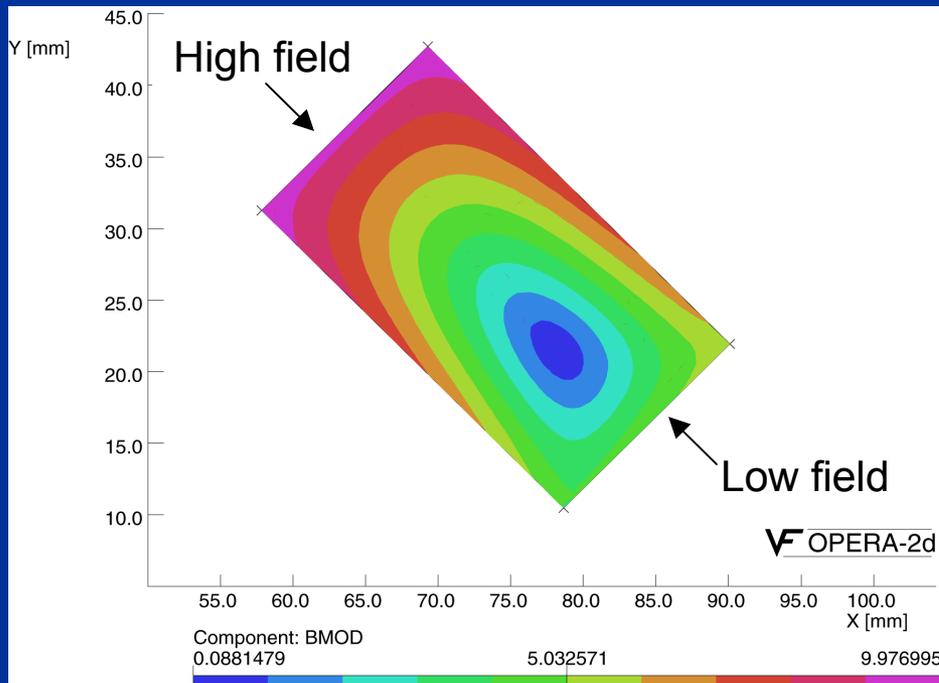
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# Lorentz forces

- $I = 11000 \text{ A}$
- $G = 95 \text{ T/m}$
- $B = \sim 10 \text{ T}$
- $F_g = 1210 \text{ N/mm}$
- $F_r = 150 \text{ N/mm}$
- $\sigma_{g\text{coil}} = 80 \text{ MPa}$



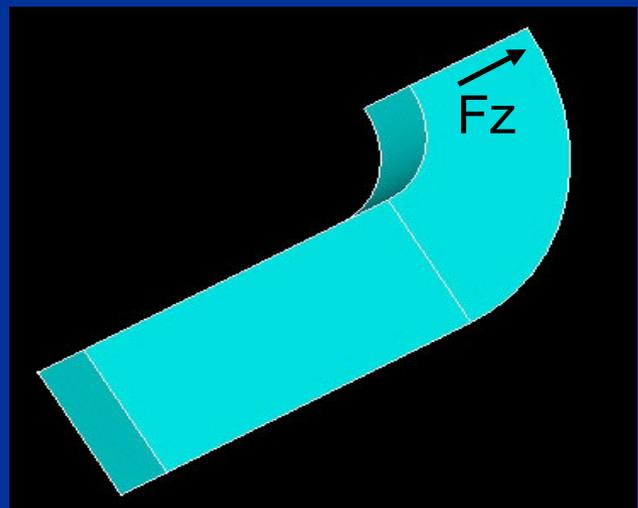
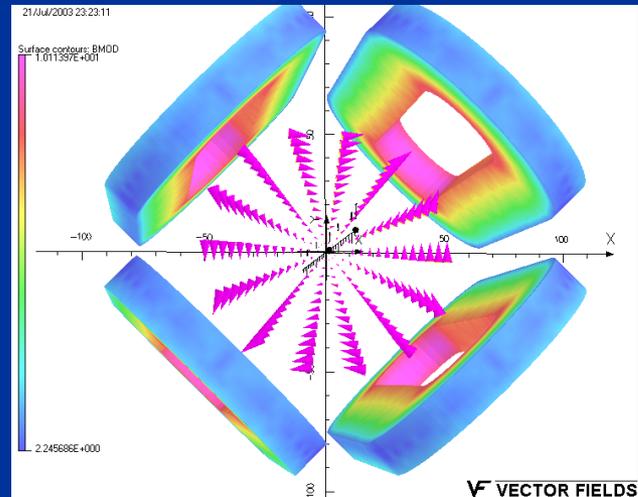
# Field and stress in the conductor



- **High stress** point close to the mid-plane
- **High field** point close to the island

# Field and forces in the end region

- **Peak field** in the end region close to the island
  - $B = \sim 11$  T at 11000 A
- Magnet **limited** by ends
- Axial Lorentz **force**:
  - $F_z = 90$  kN per coil



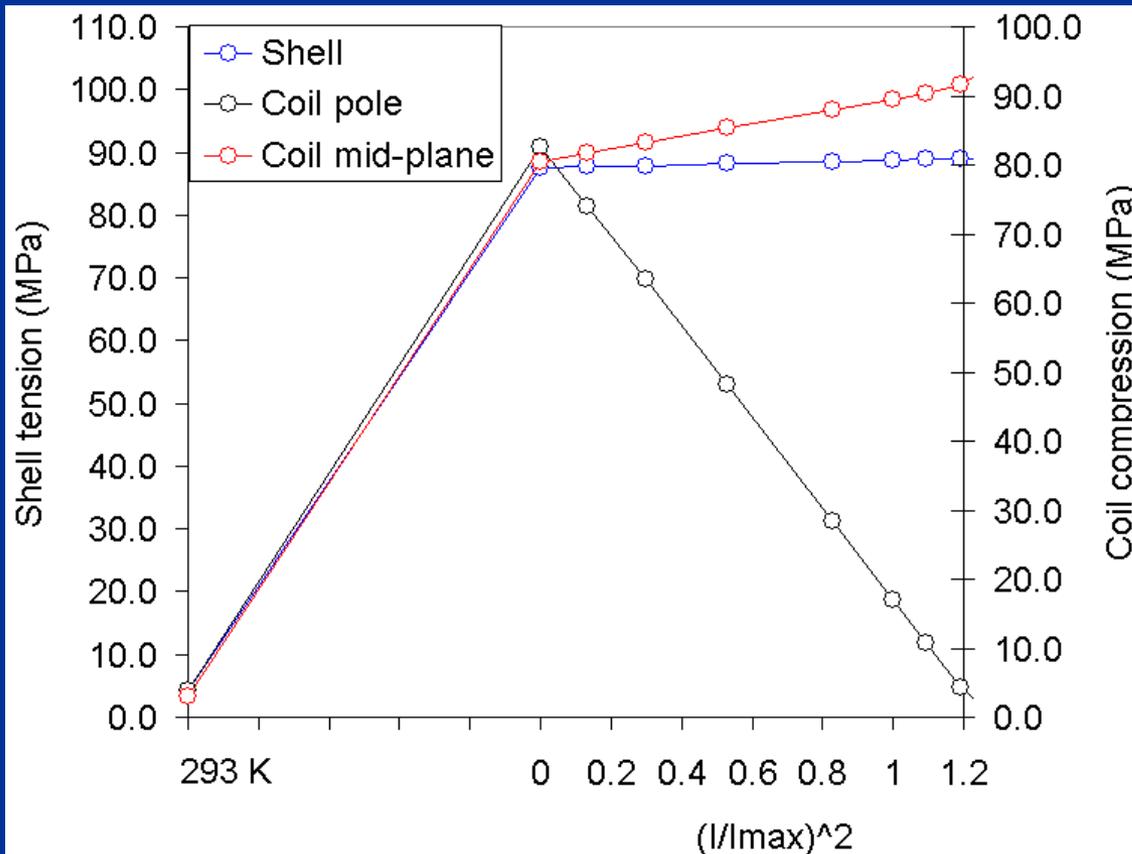


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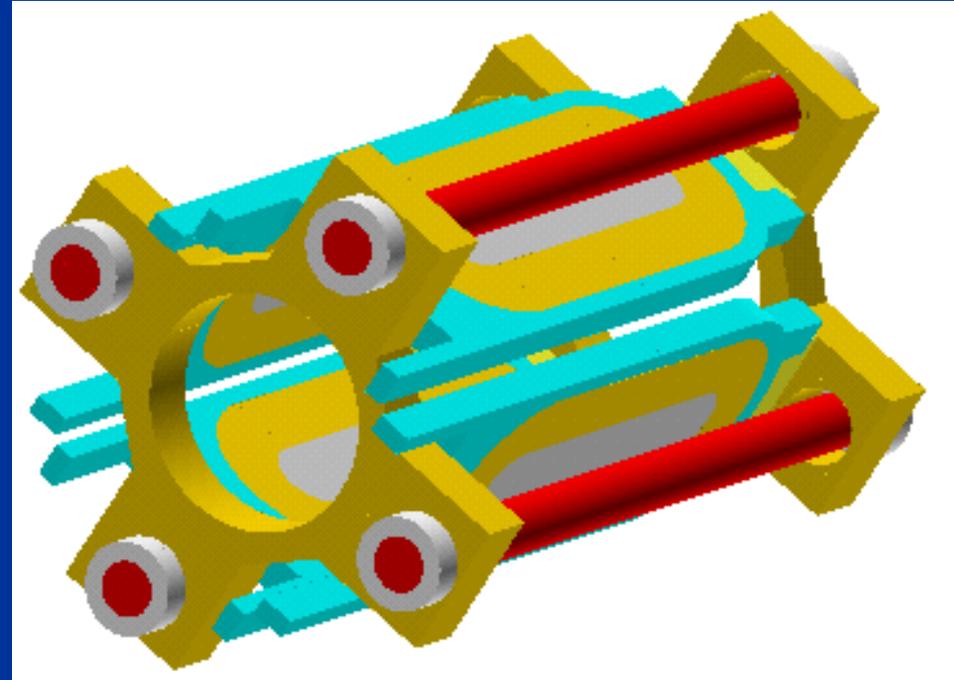
# Stress in the shell and in the coil



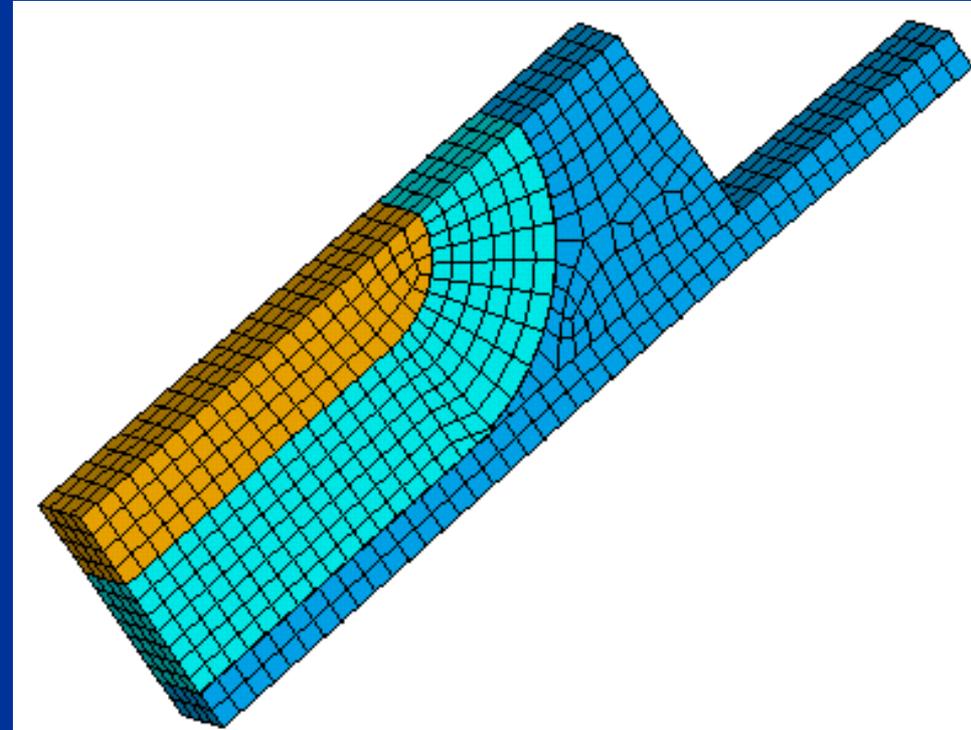
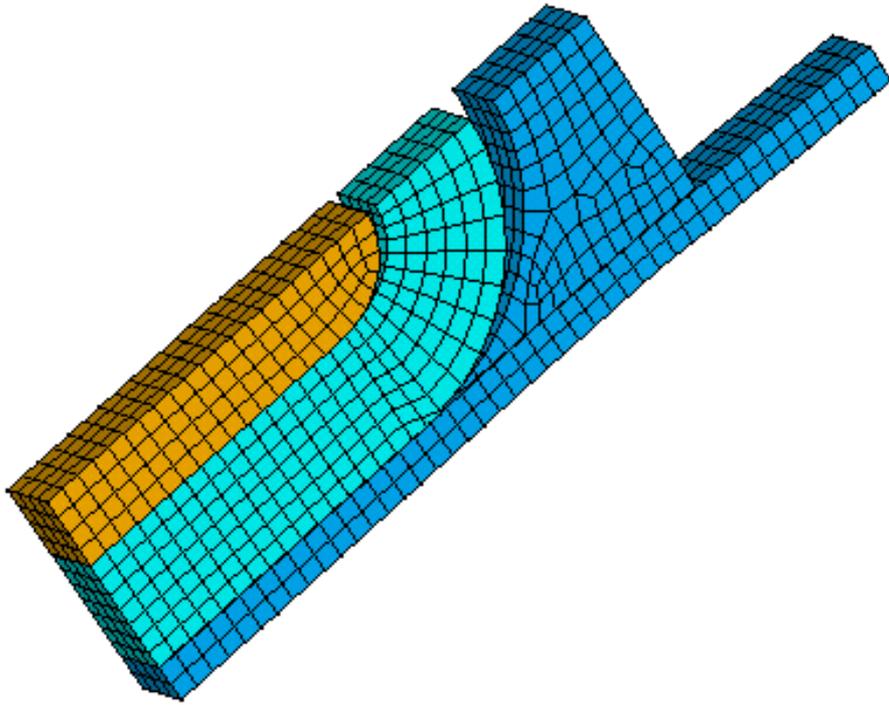
- **Low stress** at 293 K
- **Stress increase** during cool-down
- During excitation:
  - Shell stress **almost constant**
  - Pole **unloading**
  - Mid-plane **loading**
- Possible to check coil stress limits

# Axial support

- Stainless steel *end plate*
- Aluminum *rod*
  - Increase of *tension* during cool-down
  - *Axial support* during magnet excitation
- *3D pre-stressing* already implemented in HD1



# Deformation of the coil end region (full field)



- Without axial support
- Gap island-coil:  $\sim 100 \mu\text{m}$

- With axial support
- No gap island-coil



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# Conclusions

- **Feedback** for IRQ R&D and **technology development**
- **SM quadrupole magnet test** with existing coils
  - 110 mm bore with 11 T in the conductor
  - 100 MPa of coil azimuthal stress with axial support
  - Quadrupole assembly
  - Training, thermal and quench studies
  - Alignment and fabrication tolerances analysis
  - Validation of mechanical analysis
- **Schedule**
  - Assembly and test by June 2004